

SYTBL2 / Notes

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'Thermodynamic Table for Performance
Calculations in Gas Turbine Engine'
[IGTC2003Tokyo TS-093]

[SYTBL2/ Summary]

- Thermodynamic Table integrated with Flow Function Table to cover;
 - ① Temperature; T=0 – 5000 (K)
 - ② Fuel-Air Ratio; F/A = Air – Stoichiometric {F/A < 0.06824}
 - ③ Mach Number; 0 – 25
 - ④ Systems of Units; S I, Metric, British
 - ⑤ Constant κ ; (for educational purpose)
- VB Version for Hand Calculation.
- The Program written in Fortran for a Sub-routine Program.
- Dissociation was not taken into account.

Introduction

A subroutine program,, named as ‘SYTBL2’, was arranged for programming works relating to performance calculations in turbomachineries. This study on ‘SYTBL’ was presented in the IGTC’03Tokyo, of which the coefficients for the temperature less than 200(K) has been revised in ‘SYTBL2’ by using the JANAF table as shown in p.14. This notes are a guide to explain how to use the subroutine program, ‘SYTBL2.for’ in a main programming work.. The reference files will be contained in ‘ExSY2.lzh’, as shown in Table 1.

[Hand Cal.] Visual Basic version of the ‘SYTBL2’ shown in [Fig. 1]/p.3, was arranged for the convenience to hand calculations. The attached files ’ExSY2’ contains the folder [VB] which has three files in it.. Move the folder [VB] to an appropriate place in your PC, then click SYTBL2.exe, so that it will start to work. Firstly, Unit and Option button to be chosen.. The upper half is for thermodynamic table and lower half for flow function table. Viscosity; μ is also shown in Air-option. To clarify the too small or big values, .‘Exponential’ expression is arranged as shown in [Fig-1].

[Programming /Symbols] The ‘SYTBL2’ consists of two functions, i.e. Thermodynamic table [Table 12]/p.11 and Flow function table [Table 14]/p.12. To utilize the subroutine program :‘SYTBL2.for’, the format shown in [Table-11]/p.10 have to be added into the top of main program. Practically, it will be done by means of copy & paste to main program from the listing of CPCAL1, for example.

Compiling of main program will be done as:

```
C::¥MSDEV¥BIN>fl32 a:¥ Main.for a;¥Sytbl2.for.
```

The related files will be attached in the folder; [ExSY2]. The examples of utilizing thermodynamic table are shown in CPCAL1 [Table 4]/p.7, CPCAL [Table 6]/p.8 and CPCHK1 [Table 7]/p.8.

And, FLCAL1 [Table 8]/p.9, FLCAL [Table 9]/p.9 and FLCHK [Table 10]/p.10 are for the examples of flow function table. All these files are operative on DOS prompt. The listings of the attached programs will explain how to call these sub-functions.

[Tables] The Air Table [Table 20] corresponds to CPAIR1.exe, similarly Cp Table [Table 21] to CPTBL1.exe and Flow Table [Table 22] to FLTBL1.exe. By modifying those listings slightly, any tables required will be generated.

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Table 1 Attached Files ---The all files in (A),(B) are operative on DOS Prompt

[1] Hand Cal. SYTBL2.exe-----(Fig. 1) SY6UNST.log ReadMe.txt	(A) Thermodynamic Table CPCAL1.for CPCAL1.exe-----(Table 4) CPCAL.for CPCAL.exe-----(Table 6) CPCHK1.for CPCHK1.exe-----(Table 7)	[4] Tables CPAIR1.ans-----(Table 20) CPAIR1.for CPAIR1.exe
[2] Subroutine Program SYTBL2.for	(B) Flow Function Table FLCAL1.for FLCAL1.exe-----(Table 8) FLCAL.for FLCAL.exe-----(Table 9) FLCHK.for FLCHK.exe-----(Table 10)	 CPTBL1.ans-----(Table 21) CPTBL1.for CPTBL1.exe

[1] Hand Cal.

[1-1] VB-Version / Symbols

VB-Version [Fig. 1] is arranged for Hand Cal.

Upper side=Thermodynamic table.

Lower side=Flow function table.

• Unit (SI, Metric or British) and

Option (Gas, Air or κ) to be chosen first.

Option κ is for the Cal. with $\kappa=\text{Const.}$

Flow Function table

Mn ; Mach number

Ps/Pt; Pressure ratio (static to total)

Pt/Ps; Pressure ratio (total to static)

Ts/Tt; Temperature ratio (static to total)

Rs/Rt= ρ_s/ρ_t ; Density ratio (static to total)

V/Sqr(T)= V/\sqrt{T} , Velocity normalized

$Q=G\sqrt{T}/AP_t$; Volume flow rate normalized

(total, subsonic)

$S=G\sqrt{T}/AP_t$; Volume flow rate normalized

(total, supersonic)

$Q_s=G\sqrt{T}/AP_s$; Volume flow rate normalized

(static, subsonic)

A/Ach; Area ratio (Laval nozzle, subsonic)

$S=A/Ach$; Area ratio (Laval nozzle, for supersonic)

Cpm; Specific heat (mean)

κ_m ; Specific heat ratio (mean)

Thermodynamic table

T; Temperature

H; Enthalpy

U; Internal energy

Pr; Relative pressure

Vr; Relative volume

F/A; Fuel/Air ratio

Cp; Specific heat

ϕ ; Entropy function

κ ; Specific heat ratio

The screenshot shows a software application with two main panels. The top panel is titled 'Thermodynamic table' and contains input fields for Temperature (T), Specific Heat (Cp), and other thermodynamic properties like Enthalpy (H), Entropy (phi), and Specific Heat Ratio (kappa). The bottom panel is titled 'Flow Function table' and contains input fields for Mach number (Mn), Pressure ratios (Ps/Pt, Pt/Ps), and other flow properties like Velocity (V), Density (rho), and Area ratios (A/Ach).

Thermodynamic Table Inputs	Flow Function Table Inputs
T: 300	Mn: 0.5
Cp: 1.0038	T (T): 1000
H: 300.23	F/A (F): 0.0
phi: 6.7022	Ps/Pt: 0.84878
kappa: 1.4004	Pt/Ps: 1.1781
F/A: 0	Cpm: 1.1372
Pr: 1.3877	Ts/Tt: 0.95946
Vr: 216.1745	Ts: 959.46
U: 214.12	Km: 1.3375
kappa-1/kappa: .28593	A/Ach: 1.3442
Exp.(I)	

Fig. 1 VB- Version

Fuel/Air Ratio; F

- Fuel/Air ratio :F will be taken as shown in [Table 2] ,depending upon the values inputted.

Table 2 Fuel/Air Ratio; F

①; $F = f/a$ -----for $0 \leq F < 0.1$ ②; $F = \phi \equiv (f/a) / (f/a)_{st}$ -----for $0.1 \leq F \leq 1.4$ ③; $F = a/f$ ----- for $1.4 < F$
--

Three Systems of Units

- The SYTBL works for the three systems of units, SI , Metric and British, as shown below.

Table 3 Three Systems of Units

ND	1	2	3
Unit	S I	Metric	<u>British</u>
A	cm ²	cm ²	in ²
Cp, Cv, ϕ	kJ/kg K	kcal/kg K	Btu/lb R
G	kg/sec	kg/sec	lb/sec
h, u	kJ/kg	kcal/kg	Btu/lb
L	m	m	ft
P	MPa	kg/cm ²	lb/in ² (psi)
T	K	K	R
V	m/sec	m/sec	ft/sec
$\frac{V}{\sqrt{T}}$	$\frac{m/sec}{\sqrt{K}}$	$\frac{m/sec}{\sqrt{K}}$	$\frac{ft/sec}{\sqrt{R}}$
$q, q_s = \frac{G\sqrt{T}}{A P}$	$\frac{(kg/sec)\sqrt{K}}{cm^2 MPa}$	$\frac{(kg/sec)\sqrt{K}}{cm^2 kg/cm^2}$	$\frac{(lb/sec)\sqrt{R}}{in^2 psi}$

Viscosity of Air ; μ

The units for the viscosity of air ; μ are defined as below.

--- see Sec. [3-6], p. 18---

S I Unit; [Pa sec] Metric Unit; [$kg_f sec/m^2$] British Unit; [$lb_f sec/ft^2$]
--

κ = Const. Option --- See [Ex.2]/p.6---

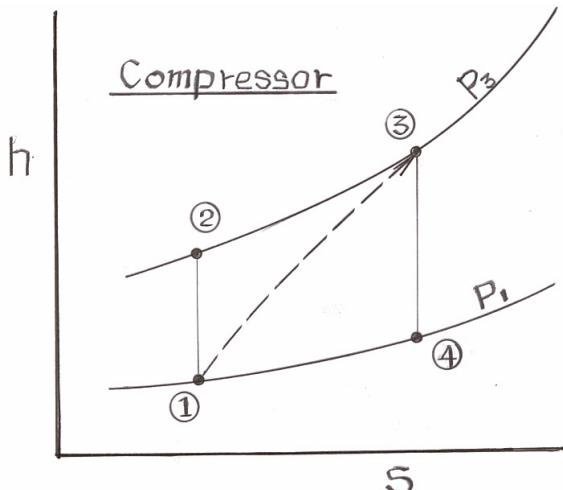
- It works for the input value of: $\kappa > 1.0$.

[1-2] Example cal.

[Ex.-1] Relative Pressure; Pr

Obtain efficiency; η of the air compressor operating at:

$$---- T_1 = 288.15, P_1 = 0.101325, \frac{P_3}{P_1} = 5.0, T_3 = 530.0 \text{ (K)} ---$$



Notes on Pr Cal.

Data given; T_1, P_1, T_3, P_3
 $h_3 = f(T_3)$

At T_1 ; $h_1 = f(T_1), \Pr_1 = f(T_1)$
 $\Pr_2 = \Pr_1 * (\frac{P_3}{P_1})$

At \Pr_2 ; $h_2 = f(\Pr_2)$

Efficiency; $\eta = (h_2 - h_1) / (h_3 - h_1)$

Compressor Efficiency Cal., ND=1 (S I unit)						
Stn.	T	P	h	ϕ	Pr	s
1	① 288.15	0.101325	288.33	6.66174	1.2052	7.31887
2	455.26	0.506625	457.21	7.12366	② 6.0260	7.31884
3	③ 530.00	0.506625	534.03	7.27987	10.3838	7.47505
4	336.60	0.101325	337.02	6.81790	④ 2.07676	7.47504

Station Cal.

- ① (Stn1); $T = 288.15 \text{ (K)}$
- ② (Stn2); $\Pr_2 = \Pr_1 * (\frac{P_3}{P_1}) = 1.2052 * 5 = 6.026$
- ③ (Stn3); $T_3 = 530. \text{ (K)}$
- ④ (Stn4); $\Pr_4 = \Pr_3 * (\frac{P_3}{P_1}) = 10.3838 / 5 = 2.07676$

Output Cal.

Adiabatic efficiency: $\eta = (h_2 - h_1) / (h_3 - h_1) = (457.21 - 288.33) / (534.03 - 288.33) = 168.88 / 245.70 = 0.6873$

Input energy = $h_3 - h_1 = 534.03 - 288.33 = 245.70 \text{ (kJ/kg)}$

Potential energy = $h_3 - h_4 = 534.03 - 337.02 = 197.01 \text{ (kJ/kg)}$

Loss energy = Input energy - Potential energy = $245.70 - 197.01 = 48.69 \text{ (kJ/kg)}$

Loss Energy / Check Cal.; [s=entropy, ϕ = Entropy function]

$$S_1 = \phi_1 - R * \ln(P_1) = \phi_1 - R * \ln(0.10132) = 6.66174 - 0.28703 * (-2.2894) = 7.31887 \text{ (kJ/kg K)}$$

$$S_3 = \phi_3 - R * \ln(P_3) = 7.27987 - 0.28703 * \ln(0.506625) = 7.47505 \text{ (kJ/kg K)}$$

$$\Delta S = S_3 - S_1 = 7.47505 - 7.31887 = 0.15618 \text{ (kJ/kg K)}$$

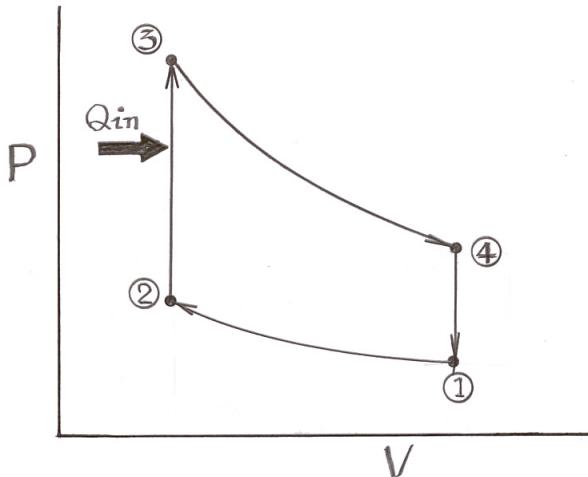
$$T_m = (T_1 + T_4) / 2 = (288.15 + 336.60) / 2 = 312.375 \text{ (K)}$$

$$\text{Loss Power} = G * T_m * \Delta S = 1.0 * 312.375 * 0.15618 = 48.78 \text{ (kJ/kg)}$$

[Ex.-2] Relative Volume; V_r ($\kappa = 1.2$)

Obtain the efficiency; η of an engine operating at;

$$--- T_1 = 288.15, P_1 = 0.101325, \varepsilon = 10., Q_{in} = 1000 ---$$



Notes on V_r Cal.

Data given; $T_1, P_1, \varepsilon, Q_{in}$

At ①; $U_1, V_{r1} = f(T_1), V_{r2} = V_{r1} / \varepsilon$

At ②; $U_2 = f(V_{r2}), U_3 = U_2 + Q_{in}$

At ③; $V_{r3} = f(U_3), V_{r4} = V_{r3} * \varepsilon$

At ④; $U_4 = f(V_{r4})$

$$W_{out} = (U_3 - U_4) / (U_2 - U_1)$$

$$\eta = W_{out} / Q_{in}$$

$$h = U_4 + R * T_1$$

$$T_6 = f(h_6)$$

*** Piston Engine Cycle Cal with $K=1.2, ND=1$, (SI unit) ***

Stn.	T (K)	P (MPa)	h	u	ϕ	Pr	V_r	SS	v=RT/1000P
1	① 288.15	0.10132	496.22	413.52	10.7534	1.3779	209.117	11.41110	0.81630
2	456.67	1.60580	786.46	655.38	11.5465	21.8377	② 20.9117	11.41041	0.08163
3	1153.46	4.05594	1986.45	③ 1655.38	13.1422	5670.3150	0.203	12.73991	0.08163
4	727.78	0.25590	1253.36	1044.46	12.3491	357.7609	④ 2.0342	12.74061	0.81629
6(Exh)	654.50	0.10132	⑤ 1127.17	939.30	12.1663	189.2562	3.458	12.82401	1.85412

$$*** \text{ (5) Exhaust Gas: } h_6 = U_4 + P_1 V_1 = U_4 + RT_1 = 1044.46 + 0.287(288.15) = 1044.46 + 82.707 = 1127.167 \text{ (kJ/kg) ***}$$

Station Cal.

- ① (Stn1); $T = 288.15 \text{ (K)}$
- ② (Stn2); $V_{r2} = V_{r1} / \varepsilon = 209.117 / 10 = 20.9117$
- ③ (Stn3); $U_3 = U_2 + Q_{in} = 655.38 + 1000 = 1655.38 \text{ (kJ/kg)}$
- ④ (Stn4); $V_{r4} = V_{r3} * \varepsilon = 0.20342 * 10 = 2.0342$

Output Cal.

$$\text{Compression Work} = U_2 - U_1 = 655.38 - 413.52 = 241.86 \text{ (kJ/kg)}$$

$$\text{Expansion Work} = U_3 - U_4 = 1655.38 - 1044.46 = 610.92 \text{ (kJ/kg)}$$

$$\text{Engine Output} = \text{Exp.W} - \text{Comp.W} = 610.92 - 241.86 = 369.06 \text{ (kJ/kg)}$$

$$\text{Thermal Efficiency} = \text{Output/Input} = 369.06 / 1000 = 0.36906$$

$$(\text{Note}): \text{Efficiency} = 1 - i / \varepsilon^{(1.2-1)} = 1 - 1 / 10^{0.2} = 1 - 0.63096 = 0.36904$$

Pressure Cal.

$$P_2 = P_1 * (P_{r2}/P_{r1}) = 0.10132 * (21.8377 / 1.3779) = 1.6058 \text{ (MPa)}$$

$$P_3 = P_2 * (T_3/T_2) = 1.6058 * (1153.46 / 456.67) = 4.05594 \text{ (MPa)}$$

$$P_4 = P_3 * (P_{r4}/P_{r3}) = 4.05594 * (357.7609 / 5670.315) = 0.2559 \text{ (MPa)}$$

Energy Balance

$$\text{Energy-In} = h_1 + Q_{in} = 496.22 + 1000 = 1496.22 \text{ (kJ/kg)}$$

$$\text{Energy-Out} = \text{Output} + h_6 = 369.06 + 1253.36 = 1496.22 \text{ (kJ/kg)}$$

$$\text{Entropy; } S = f(\phi, P), \text{ --- } \phi = \text{entropy function}$$

$$S = \phi - R * \ln(P) = \phi - 0.2870277 * \ln(P) \text{ --- for ND=1 (SI unit)}$$

$$S = \phi - R_C * \ln(P) = \phi - 0.0685554 * \ln(P) \text{ --- for ND=2 (Metric unit) and ND=3 (British unit)}$$

[2] Programming / Symbols

[2-1] Example Calculations.(Operative on DOS Prompt)

[Ex.-1] **CPCAL1** ---Thermodynamic table for [CK=0.0, ND=1]

INPUT DATA

I = Option No.

- = 1, T: Temperature [K]
- = 2, H: Enthalpy [kJ/kg]
- = 3, U: Internal energy [kJ/kg]
- = 4, Pr: Relative pressure
- = 5, Vr: Relative volume

F = Fuel/ Air ratio—see [Table 5]

OUTPUT DATA

Table 4 shows the output for;
[I=1 , T= 300 (K), F=0.]

Table 4 Example. Cal./ CPCAL1

```
C:¥FOR¥BINB>CPCAL1
I, ( T: H: U: Pr: Vr ), F ???
1 300 0.0

T= 300.000  CP=1.003821  H= 300.235  VR=.21617E+03  U = 214.126
F/A= .00000  K = 1.40043  PHI= 6.70222  PR= .1388E+01  (K-1)/K=.285935
```

Notes:

(1) The options in CPCAL1 are defined as [CK=0.0, ND=1]. The CK stands for Constant Kappa Option, If CK=1.3 inputted, the table will show the characteristics for $\kappa = 1.3$.

(2) The option: ND stands for Number of Dimensions.

ND=1 for SI unit, ND=2 for Metric unit and ND=3 for British unit.

(3) F stands for Fuel / Air ratio which will be taken as below depending upon the value inputted.

Table 5 Fuel/Air Ratio

$F = f / a$	for $0 \leq F < 0.10$
$F = \phi \equiv f/a / (f/a)_{st}$	for $0.10 \leq F \leq 1.4$
$F = a / f$	for $1.4 < F$

That is, $F=0.06825 - (f/a)$, $F=1.0 - (f/a)_{st}$ and $F=14.653 - (a/f)$, all for the characteristics at Stoichiometric Condition, same meaning..

(4) There are examples utilizing the following sub-functions of Thermodynamic functions in the listins of ‘CPCAL1.for’.

CPT, HFT, SFT, UFT, PRT, and VRT.

[Ex.-2] CPCAL ---Thermodynamic table

Table 6 Example Cal. / CPCAL (Operative on DOS prompt)

C:¥FOR¥BINB>CPCAL

CK, ND, I, (T: H: U: Pr: Vr), F ???
0.0 1 2 300.235 0.0

T= 300.000 CP=1.003821 H= 300.235 VR= .21617E+03 U = 214.127
F/A= .00000 K = 1.40043 PHI= 6.70222 PR= .1388E+01 (K-1)/K=.285935

Notes

- (1) CPCAL[Table 6] is the same program as CPCAL1[Table 4], but the options of CK and ND are arranged as input data. in CPCAL. [Table 6] shows the characteristics corresponding to the enthalpy of: h=300.235 by using the option :I=2.
- (2) Option [CK=0.0, ND=1] were chosen for CPCAL1 in the listing of CPCAL.for.

[Ex.-3] CPCHK1 ---Thermodynamic table for [CK=0.0, ND=1]

Table 7 Example Cal./ CPCHK.1

C:¥FOR¥BINB>CPCHK1

T, F ???
300 0.0
T= 300.000 CP=1.003821 H= 300.235 VR= .2162E+03 U = 214.126
F/A= .00000 K = 1.400433 PHI= 6.70222 PR= .1388E+01 (K-1)/K=.285935

(5) TFH	H=	300.234500	T=	300.000000
(6) TPR	PR=	1.387768	T=	300.000000
(9) TFU	U=	214.126200	T=	300.000000
(14) TVR	VR=	216.174500	T=	300.000000
(10) HVR	VR=	216.174500	H=	300.234500
(11) HPR	PR=	1.387768	H=	300.234500
(12) UPR	PR=	1.387768	U=	214.126200
(13) UVR	VR=	216.174500	U=	214.126200
(15) PRH	H=	300.234500	PR=	1.387768
(18) PRU	U=	214.126200	PR=	1.387768
(16) VRH	H=	300.234500	VR=	216.174500
(17) VRU	U=	214.126200	VR=	216.174500

Note:

Thermodynamic table contains 18 sub-functions as shown in [Table 12]/ p.11.
The all sub-functions are used in CPCHK1. ---See the listings of CPCHK1.for---

[Ex.-4] **FLCAL1** (Operative on DOS prompt.) ---Flow function table [CK=0.0, ND=1]

INPUT DATA

J = Option No.	= 7, Q, volume flow rate(subsonic) $\frac{G\sqrt{T}}{AP_i}$
= 1, Mn; Mach number	
= 2, PsR; pressure ratio: Ps/Pt	= 8; Qs volume flow rate: $\frac{G\sqrt{T_i}}{AP_s}$
= 3, PtR, pressure ratio: Pt/Ps	= 9; AsR; area ratio(subsonic):A/Ach
= 4, TsR, temperature ratio: Ts/Tt	= 10; SQ: volume flow rate(supersonic) $\frac{G\sqrt{T_i}}{AP_i}$
= 5, RsR, density ratio: ρ_s / ρ_t	
= 6, VfT, velocity normalized: V/\sqrt{Tt}	= 11; SAs; area ratio(supersonic): A/Ach

OUTPUT

V/RTt; velocity normalized: V/\sqrt{Tt}

RO/ROt; density ratio: ρ_s / ρ_t

Table 8 Example Cal. / FLCAL1 ---see Table 3/p.4 for units.

C:¥FOR¥BINB>FLCAL1

J,(Mn:PsR:PtR: TsR:RsR:VfT: Q:Qs:AsR: SQ:SAsR), T, F ???

1 0.5 300 0.0

Tt= 300.000 Ts= 285.691 CPm = 1.00345 Km=1.40064 (Km-1)/Km=.28604

Mn= .500 P/Pt= .84294 Ts/T = .95230 V/RTt= 9.7839 Q = 3.01724

F/A= .00000 Pt/P= 1.1863 RO/ROt= .88516 A/At= 1.3397 Qs= 3.57943

[Notes]

(1) FLCAL1 is the table for [CK=0.0, ND=1], i.e. for SI unit.

(2) [Table 8] shows the flow table for the INPUT DATA: J=1(Mn), Mn=1, T=300(K), F=0.0(Air).

[Ex. 5] **FLCAL** (Operative on DOS prompt.)---Flow function table

Table 9 Example Cal. / FLCAL

C:¥FOR¥BINB>FLCAL

CK,ND,J,(Mn:PsR:PtR: TsR:RsR:VfT: Q:Qs:AsR: SQ:SAs R), T, F ???

0.0 1 1 0.5 300. 0.0

Tt= 300.000 Ts= 285.691 CPm = 1.00345 Km=1.40064 (Km-1)/Km=.28604

Mn= .500 P/Pt= .84294 Ts/T = .95230 V/RTt= 9.7839 Q = 3.01724

F/A= .00000 Pt/P= 1.1863 RO/ROt= .88516 A/At= 1.3397 Qs= 3.57943

[Note] Options ; CK and ND are arranged as INPUT DATA in FLCAL/Table 9.

[Ex-6] **FLCHK**(Operative on DOS prompt) ---Flow function check program

Flow function table consists of 9 sub-functions as shown in [Table 14]/ p.12.
The all sub-functions are used in FLCHK. ---See the listings of FLCHK.for.

Table 10 Example Cal. / FLCHK

C:¥FOR¥BINB>FLCHK
CK, ND, Mn, T ,F ???
0.0 1 0.5 300. 0.0
Tt= 300.000 Ts= 285.691 CPm = 1.00345 Km=1.40064 (Km-1)/Km=.28604
Mn= .500 P/Pt= .84294 Ts/T = .95230 V/RTt= 9.7839 Q = 3.01724
F/A= .00000 Pt/P= 1.18632 RO/ROt= .88516 A/At= 1.3397 Qs= 3.57943
(22) PSR; PSPT= 8.429400E-01 Mn = 5.000015E-01
(23) PTR; PTPS= 1.186324 Mn = 5.000015E-01
(24) TSR; TSTT= 9.523023E-01 Mn = 4.999910E-01
(25) RSR; RSRT= 8.851597E-01 Mn = 5.005257E-01
(26) VFT; VRT= 9.783910 Mn = 5.000523E-01
(27) FQT; Q = 3.017244 Mn = 4.999988E-01
(28) FQS; QS = 3.579430 Mn = 5.000289E-01
(29) ASR; ASR = 1.339727 Mn = 5.000005E-01

[Ex.-7] **Format**

Table 11 Format

\$DEBUG
COMMON/SYIAE/RC,R,AFST,CK,ND,G,CJK,AKR
COMMON/SHEN/TSX,CPMX,AKMX,AKRMX
COMMON/YANG/AMNX,PSPTX,PTPSX,TSTTX,RSRTX,VRTX,QX,QSX,ASATX
C
UR=8.31433 ! (kJ/kmol K)
AM=28.967 ! (kg/kmol)
G=9.80665
CJK=4.1868 ! (kJ/kcal)
R=UR/AM !=0.2870277 (kJ/kg K)
RC=R/CJK !=0.0685554 (kcal/kg K) or (Btu/lb R)
ND=1 ! ND=1 for SI, 2 for Metric , 3 for British

[2-2] Subroutine / Formats

'SYTBL2' consists of two tables; Thermodynamic table and Flow-function table.

(1) Thermodynamic Table

Thermodynamic table consists of 18 sub-functions. — [Table 13] .

Table 12 Thermodynamic table / Function Names

		To Obtain						
		T	Cp	h	Φ	u	Pr	Vr
From	T	① CPT	② HFT	③ SFT	⑦ UFT	④ PRT	⑧ VRT	
	Cp							
	h	⑤ TFH				⑯ PRH	⑯ VRH	
	Φ							
	u	⑨ TFU				⑮ PRU	⑮ VRU	
	Pr	⑥ TPR		⑪ HPR		⑫ UPR		
	Vr	⑭ TVR		⑩ HVR		⑬ UVR		

Table 13 Thermodynamic table / Formats

No	Functions	Names	Related
1	$Cp=f(T)$	CPT(T, F, Cp, AK)	--
2	$h=f(T)$	HFT(T, F, H)	--
3	$S=f(T)$	SFT(T, F, S)	--
4	$Pr=f(T)$	PRT(T, F, Pr)	(3)
5	$T=f(h)$	TFH(H, F, T)	(2)
6	$T=f(Pr)$	TPR(PR, F, T)	(4)
7	$U=f(T)$	UFT(T, F, U)	(2)
8	$Vr=f(T)$	VRT(T, F, Vr)	(4)
9	$T=f(U)$	TFU(U, F, T)	(5)

No	Functions	Names	Related
10	$h=f(Vr)$	HVR(VR, F, H)	(2), (8)
11	$h=f(Pr)$	HPR(PR, F, H)	(2), (6)
12	$U=f(Pr)$	UPR(PR, F, U)	(6), (7)
13	$U=f(Vr)$	UVR(VR, F, U)	(7), (14)
14	$T=f(Vr)$	TVR(VR, F, T)	(5), (10)
15	$Pr=f(h)$	PRH(H, F, Pr)	(5), (9)
16	$Vr=f(h)$	VRH(H, F, Vr)	(5), (8)
17	$Vr=f(U)$	VRU(U, F, Vr)	(8), (9)
18	$Pr=f(U)$	PRU(U, F, Pr)	(4), (9)

(Note) The values written in red are for the characteristics to be obtained.

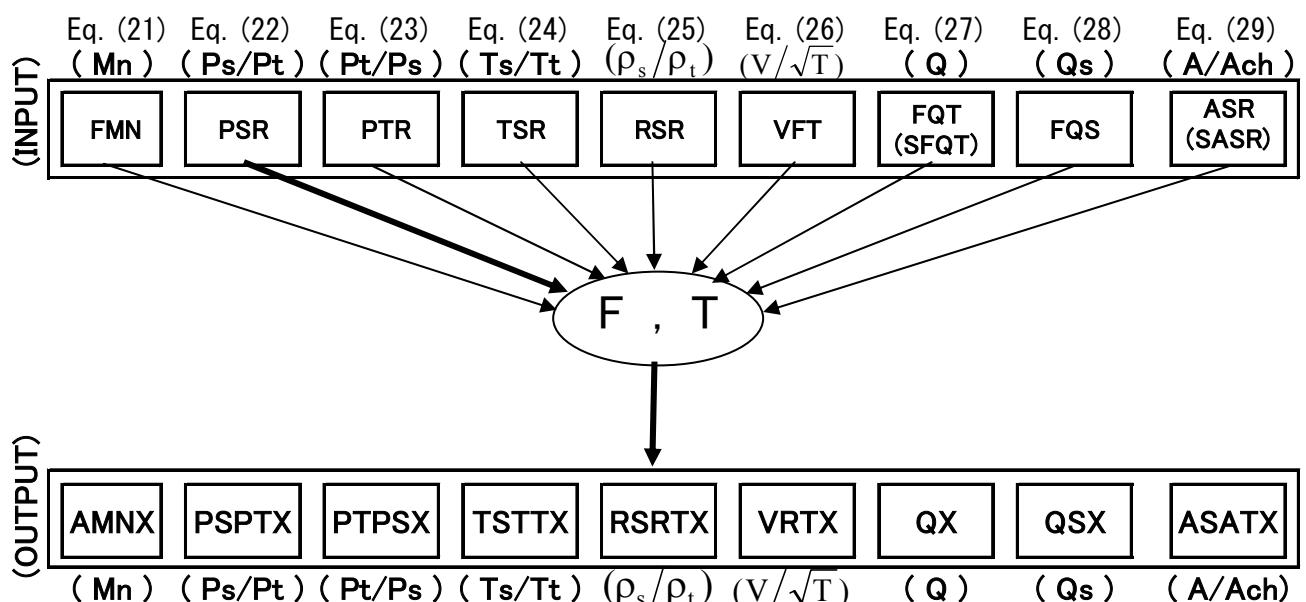
(2) Flow-Function Table

Flow-function table consists of 9 sub-functions. — [Table 14] .

Table 14 Function Names & OUTPUT

Eq. No.	Input Format		Output Format ; (Y)	
	Equation	Formats	Output	Symbols
2 1	$Y = f(M_n)$	FMN (M_n, F, T)	M_n	AMNX
2 2	$Y = f(P_s/P_t)$	PSR ($P_s/P_t, F, T$)	P_s/P_t	PSPTX
2 3	$Y = f(P_t/P_s)$	PTR ($P_t/P_s, F, T$)	P_t/P_s	PTPSX
2 4	$Y = f(T_s/T_t)$	TSR ($T_s/T_t, F, T$)	T_s/T_t	TSTTX
2 5	$Y = f(\rho_s/\rho_t)$	RSR ($\rho_s/\rho_t, F, T$)	ρ_s/ρ_t	RSRTX
2 6	$Y = f(V/\sqrt{T_t})$	VFT ($V/\sqrt{T_t}, F, T$)	$V/\sqrt{T_t}$	VRTX
2 7	$Y = f(Q_t)$	FQT (Q_t, F, T) SFQT (Q_t, F, T)	Q_t	QX
2 8	$Y = f(Q_s)$	FQS (Q_s, F, T)	Q_s	QSX
2 9	$Y = f(A/Ach)$	ASR ($A/Ach, F, T$) SASR (M_n, F, T)	A/Ach	ASATX

Table 15 Flow-function table /Schematics



[3] Related Equations

[3-1] Constants

Universal gas constant; UR=**8.31433** [kJ/kmol K]

Molecular weight of air ; M=**28.967** [kg/kmol]

Acceleration of gravity; g=**9.80665** [m/sec²]

Conversion factor CJK=**4.1868** [kJ/kcal]

$$1[\text{lb}] = 0.4535924 = \mathbf{0.4536} [\text{kg}], \quad 1[\text{ft}] = \mathbf{0.3048} [\text{m}]$$

Acceleration of gravity [British]; **32.174** [ft/sec²]

$$= 9.80665 / 0.3048$$

Units;

$$1[\text{kgf}] = 9.80665 [\text{N}], \quad [\text{N}\cdot\text{m}] = [\text{J}], \quad [\text{J}/\text{sec}] = [\text{w}],$$

$$[\text{J}/\text{kg}] = [\text{m/sec}]^2$$

Gas constant;

$$R = UR/M = 8.31433/28.967 = 0.2870277$$

$$= \mathbf{(0.287)} [\text{kJ/kg K}] \text{--for SI unit.}$$

$$RC = R/CJK = 8.31433/28.967/4.1868 = 0.0685554$$

$$= \mathbf{(0.06856)} [\text{kcal/kg-K}], \text{ or } \{\text{Btu/lb-R}\} = RM/J = RB/JB$$

$$RM = UR * 1000 / M / g = 8314.33 / 28.967 / 9.80665$$

$$= 29.2691227 = \mathbf{(29.27)} [\text{kg-m/kg-K}] \text{ --Metric unit}$$

$$RB = RM / 1.8 / 0.3048 = 53.3476871$$

$$= \mathbf{(53.35)} [\text{ft-lb/lb-R}] \text{ --British unit}$$

Mechanical equivalent of heat;

$$J = CJK * 10^3 / g = 4186.8 / 9.80665 = 426.934784$$

$$= \mathbf{(426.9)} [\text{kg-m/kcal}]$$

$$JB = CJK * 10^3 / g / 1.8 / 0.3048 = 4186.8 / 0.80665 / 1.8 / 0.3048$$

$$= 778.1692622 = \mathbf{(778.2)} [\text{ft-lb/lb-R}]$$

Pressure;

$$1[\text{kg/cm}^2] = 1[\text{kg/cm}^2] * g / 100 = 9.80665 / 100$$

$$= (0.0980665) [\text{MPa}]$$

$$= 1[\text{kg/cm}^2] * 2.54^2 / 0.4535924 = 14.2233424 = \mathbf{(14.223)} [\text{psi}]$$

Standard ambient pressure;

$$P_0 = \mathbf{1.0332} [\text{kg/cm}^2] \text{ --for Metric unit}$$

$$= 1.0332 * g / 100 = 1.0332 * 9.80665 / 100 = 0.101322308$$

$$= \mathbf{(0.10132)} [\text{MPa}]$$

$$= 1.0332 * 2.54^2 / 0.4535924 = 14.6955573 = \mathbf{(14.696)} [\text{psi}]$$

Entropy; s at T₀, P₀ (Standard ambient condition.)

$$[\text{SI}]; s = \phi - R * \ln(P) = 6.66174 - 0.287 * \ln(0.10132)$$

$$= 6.66174 - 0.287 * (-2.2894715) = 7.31888 [\text{J/kg-K}]$$

$$[\text{Metric}]; s = 1.59112 - RC * \ln(1.0332)$$

$$= 1.59112 - 0.06856 * 0.0326608 = 1.58888 [\text{kcal/kg-K}]$$

$$[\text{British}]; s = 1.59113 - RC * \ln(14.696)$$

$$= 1.59112 - 0.06856 * 2.6875753 = 1.40689 [\text{Btu/lb-R}]$$

Specific Weight; γ

— at T₀, P₀ (Standard Ambient Condition.)

$$[\text{SI}] \gamma = P / (R * T) = 0.101322 * 10^3 / 0.287 / 288.15$$

$$= \mathbf{1.2251} [\text{kg/m}^3]$$

$$[\text{Metric}] \gamma = P / (RM * T) = 1.0332 * 10^4 / 29.27 / 288.15$$

$$= \mathbf{1.2251} [\text{kg/m}^3]$$

$$[\text{British}] \gamma = P / (RB * T)$$

$$= 14.696 * 144 / 53.35 / 518.67 = \mathbf{0.07648} [\text{lb/ft}^3]$$

$$(\text{Note}) ; [1\text{b/ft}^3] = 1[\text{kg/m}^3] * (0.3048)^3 / 0.4536$$

$$= 1/16.018 [\text{lb/ft}^3]$$

Horsepower;

$$[\text{Metric}] PS = 75 [\text{kg-m/sec}]$$

$$= 75 * g [w] = 75 * 9.80665 / 10^3 = 0.7355 [\text{kw}]$$

$$[\text{British}] HP = 550 [\text{lb-ft/sec}]$$

$$= (550 * 0.4536 * 0.3048) * 9.80665 / 10^3 = 0.7457 [\text{kw}]$$

[3-2] Thermodynamic Table

Table 16 Thermodynamic functions

$C_{pa} = C_0 + C_1 T + C_2 T^2 + C_3 T^3 + C_4 T^4 \quad \dots \dots \dots (1)$ $ha = \int_0^T C_{pd} dT \quad \dots \dots \dots (2)$ $= C_0 T + \frac{C_1}{2} T^2 + \frac{C_2}{3} T^3 + \frac{C_3}{4} T^4 + \frac{C_4}{5} T^5 + CH$ $\phi a = \int_0^T \frac{C_p}{T} dT \quad \dots \dots \dots (3)$ $= C_0 \ln(T) + C_1 T + \frac{C_2}{2} T^2 + \frac{C_3}{3} T^3 + \frac{C_4}{4} T^4 + CF$ $\theta_{cp} = (1+a)(C_{p,ST} - C_{pa}) \quad \dots \dots \dots (4)$ $\theta_h = (1+a)(h_{ST} - ha) \quad \dots \dots \dots (5)$ $\theta_\phi = (1+a)(\phi_{ST} - \phi a) \quad \dots \dots \dots (6)$	$C_p = C_{pa} + \frac{f}{1+f} \theta_{cp} \quad \dots \dots \dots (7)$ $h = ha + \frac{f}{1+f} \theta_h \quad \dots \dots \dots (8)$ $\phi = \phi a + \frac{f}{1+f} \theta_\phi \quad \dots \dots \dots (9)$ $\theta_{cp} = CP_0 + CP_1 T + CP_2 T^2 + CP_3 T^3 + CP_4 T^4 + CP_5 T^5 \quad \dots \dots \dots (10)$ $\theta_h = H_0 + H_1 T + H_2 T^2 + H_3 T^3 + H_4 T^4 + H_5 T^5 \quad \dots \dots \dots (11)$ $\theta_\phi = F_0 + FT + FT^2 + FT^3 + FT^4 + FT^5 \quad \dots \dots \dots (12)$
--	--

Where: $f = 0.06825$ at stoichiometric
 $a = 1/f = 14.652$ used for this table.

Table 17 Coefficients

Symbol	SYTBL2 / Coefficients [kJ/kg K]					Equation
	0 K - 300 K	200 K - 800 K	800 K - 2200 K	2200K - 5000 K	2005-1-19	
C_0	$B1=.1001704E+01$	$DC0=.1018913E+01$	$CD10=.7986551E+00$	$A11=.8852846E+00$		
C_1	$B2=.3383075E-05$	$DC1=-.1378364E-03$	$CD11=.5339216E-03$	$A12=.3702210E-03$		
C_2	$B3=.5877607E-08$	$DC2=.1984340E-06$	$CD12=-.2288169E-06$	$A13=-.1349033E-06$		
C_3	$B4=-.2643871E-09$	$DC3=.4239924E-09$	$CD13=.3742086E-10$	$A14=.2368343E-10$		
C_4	$B5=.1038620E-11$	$DC4=-.3763249E-12$	$CD14=.0000000E+00$	$A15=-.1580984E-14$		
CH	$B6=-.2180805E+00$	$DCH=-.1698463E+01$	$CD1H=.4738465E+02$	$A16=.1545856E+02$		2
CF	$B7=.9921631E+00$	$DCF=.9199264E+00$	$CD1F=.2019088E+01$	$A17=.1543854E+01$		3
CP_0	$G1=.7251687E-01$	$DP0=-.3594941E+00$	$CP10=.1088757E+01$	$D11=.3828289E-01$		
CP_1	$G2=.3532892E-02$	$DP1=.4516399E-02$	$CP11=-.1415883E-03$	$D12=.2714380E-02$		
CP_2	$G3=-.2248715E-04$	$DP2=.2811636E-05$	$CP12=.1916016E-05$	$D13=-.1017066E-05$		
CP_3	$G4=.1136625E-06$	$DP3=-.2170873E-07$	$CP13=-.1240093E-08$	$D14=.1722610E-09$		
CP_4	$G5=-.1622836E-09$	$DP4=.2868878E-10$	$CP14=.3016695E-12$	$D15=-.1103124E-13$		
CP_5	$G6=.0000000E+00$	$DP5=-.1222634E-13$	$CP15=-.2611711E-16$	$D16=.0000000E+00$		
H_0	$VH=.9339293E+01$	$DH0=.6263742E+02$	$DH10=-.1768385E+03$	$P16=.7008344E+02$		
H_1	$V1=.7251687E-01$	$DH1=-.5286657E+00$	$DH11=.8369064E+00$	$P11=.3828289E-01$		
H_2	$V2=.1766446E-02$	$DH2=.3222623E-02$	$DH12=.3647621E-03$	$P12=.1357190E-02$		
H_3	$V3=-.7495717E-05$	$DH3=-.2167025E-05$	$DH13=.2515545E-06$	$P13=-.3390221E-06$		
H_4	$V4=.2841561E-07$	$DH4=.2495170E-09$	$DH14=-.1254134E-09$	$P14=.4306526E-10$		
H_5	$V5=-.3245672E-10$	$DH5=.3489182E-12$	$DH15=.1640627E-13$	$P15=-.2206248E-14$		
F_0	$RA7=-.1117070E+01$	$DF0=-.7126983E+00$	$DF10=-.1264536E+01$	$QA17=-.7808500E+00$		
F_1	$RA1=.7320000E-02$	$DF1=-.2295019E-03$	$DF11=.4468673E-02$	$QA11=.2800000E-02$		
F_2	$RA2=-.4245800E-04$	$DF2=.1315413E-04$	$DF12=-.2853818E-05$	$QA12=-.5432150E-06$		
F_3	$RA3=.1826960E-06$	$DF3=-.2553182E-07$	$DF13=.1640346E-08$	$QA13=.6632280E-10$		
F_4	$RA4=-.3737920E-09$	$DF4=.2239099E-10$	$DF14=-.5314314E-12$	$QA14=-.3973220E-14$		
F_5	$RA5=.2970480E-12$	$DF5=-.7607185E-14$	$DF15=.6988461E-16$	$QA15=.6744780E-19$		

[3-3] Flow Function Table

Table 18 Flow functions

$Mn = v/a = \sqrt{2\Delta h}/\sqrt{\kappa_s RT_s}$	----- (1)	$\frac{V}{\sqrt{T_t}} = \sqrt{\kappa_s R} \frac{Mn}{\left[1 + \left(\frac{\kappa_s}{\kappa_m}\right) \left(\frac{\kappa_m - 1}{2}\right) Mn^2\right]} \quad \text{----- (6)}$
	----- (2)	
$\frac{P_s}{P_t} = \frac{1}{\left[1 + \left(\frac{\kappa_s}{\kappa_m}\right) \left(\frac{\kappa_m - 1}{\kappa_m}\right) Mn^2\right]^{\frac{\kappa_m - 1}{\kappa_m - 1}}} \quad \text{----- (7)}$		
$\frac{P_t}{P_s} = \left[1 + \left(\frac{\kappa_s}{\kappa_m}\right) \left(\frac{\kappa_m - 1}{\kappa_m}\right) Mn^2\right]^{\frac{\kappa_m - 1}{\kappa_m - 1}} \quad \text{----- (3)}$	----- (4)	
$\frac{T_s}{T_t} = \frac{1}{\left[1 + \left(\frac{\kappa_s}{\kappa_m}\right) \left(\frac{\kappa_m - 1}{\kappa_m}\right) Mn^2\right]} \quad \text{----- (5)}$		$q \equiv \left(\frac{G\sqrt{T_t}}{A P_t}\right) = 10^2 \sqrt{\frac{\kappa_s}{R}} \frac{Mn}{\left[1 + \left(\frac{\kappa_s}{\kappa_m}\right) \left(\frac{\kappa_m - 1}{2}\right) Mn^2\right]^{\frac{\kappa_m + 1}{2(\kappa_m - 1)}}} \quad \text{----- (8)}$
$\frac{\rho_s}{\rho_t} = \frac{1}{\left[1 + \left(\frac{\kappa_s}{\kappa_m}\right) \left(\frac{\kappa_m - 1}{2}\right) Mn^2\right]^{\frac{1}{\kappa_m - 1}}} \quad \text{----- (9)}$		$q_s \equiv \left(\frac{G\sqrt{T_t}}{A P_s}\right) = 10^2 \sqrt{\frac{\kappa_s}{R}} Mn \sqrt{1 + \left(\frac{\kappa_s}{\kappa_m}\right) \left(\frac{\kappa_m - 1}{2}\right) Mn^2} \quad \text{----- (9)}$

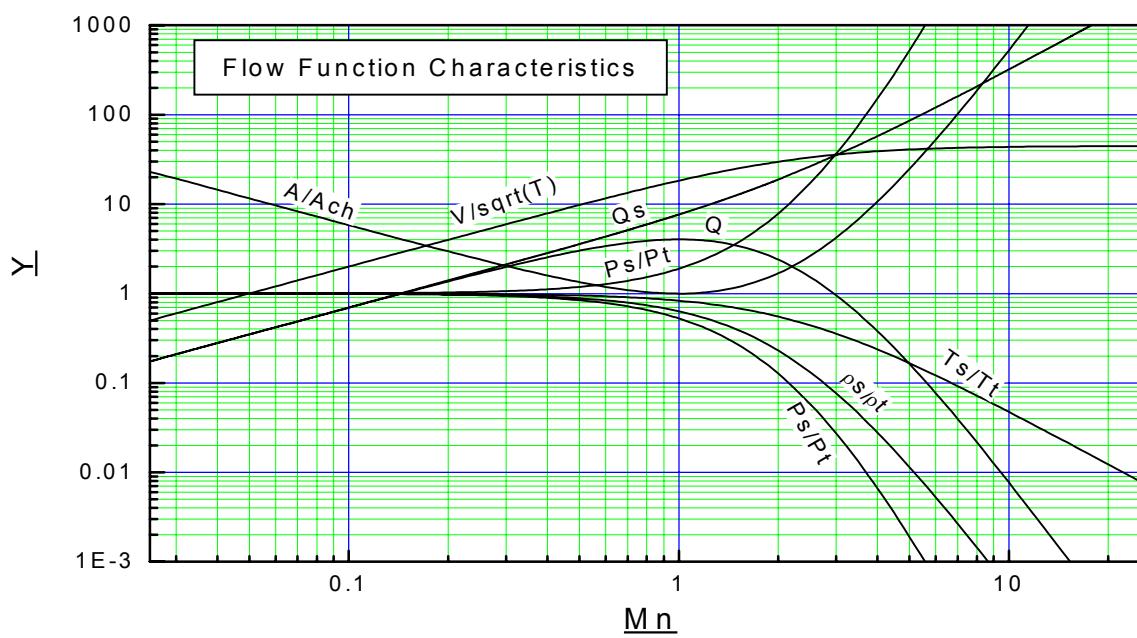


Fig. 2 Flow Functions / Characteristics

[3-4] Relative Pressure; Pr and Relative Volume; Vr

[A] Relative Pressure; Pr

From basic equations in thermodynamics:

$$dq = dh - vdp \quad \left[\frac{\text{kJ}}{\text{Kg}} \right] \quad \dots\dots(1)$$

$$ds = \frac{dq}{T} \quad \left[\frac{\text{kJ}}{\text{KgK}} \right] \quad \dots\dots(2)$$

$$\rightarrow Tds = dh - vdp \quad \dots\dots(3)$$

For $ds = 0$ in Eq.(3)

$$dh = Cp dT = vdp \quad \dots\dots(4)$$

$$pv = RT \rightarrow v = \frac{RT}{p} \quad \dots\dots(5)$$

With Eq.(5), Eq.(4) becomes:

$$Cp dT = \frac{RT}{p} dp$$

$$\rightarrow \frac{dp}{p} = \frac{1}{R} \frac{Cp}{T} dT$$

Integrating the above equation;

$$\int_0^p \frac{dp}{p} = \frac{1}{R} \int_0^T \frac{Cp}{T} dT$$

$$\ln\left(\frac{p}{p_0}\right) = \frac{1}{R} \int_0^T \frac{Cp}{T} dT = \frac{1}{R}(\phi - \phi_0) \quad \dots\dots(6)$$

Note that;

$$\phi \equiv \int_0^T \frac{Cp}{T} dT = \text{Entropy Function}$$

Put $Pr = \left(\frac{p}{p_0}\right)$ in Eq.(6), so that;

$$\ln Pr = \frac{1}{R}(\phi - \phi_0) \quad \dots\dots(7)$$

Relative pressure; Pr may be obtained from Eq.(7) as;

$$Pr = \text{Exp}\left\{\frac{1}{R}(\phi - \phi_0)\right\} \quad \dots\dots(8)$$

where; $\phi_0 \equiv \phi$ at $T_0 = 273.15 \text{ (K)}$

[B] Relative Volume; Vr

Basic equations;

$$Cp - Cv = R \quad \dots\dots(9)$$

$$dQ = du + pdv \quad \dots\dots(10)$$

$$du = Tds - pdv \quad \dots\dots(11)$$

Eq.(11) at $ds = 0$;

$$du \equiv Cv dT = -pdv \quad \dots\dots(12)$$

$$pv = RT$$

$$\rightarrow p = \frac{RT}{v} \quad \dots\dots(13)$$

Eq.(12) may be written by using Eq.(13) as;

$$Cv dT = -RT \frac{dv}{v}$$

$$\rightarrow \frac{dv}{v} = -\frac{Cv}{RT} dT \quad \dots\dots(14)$$

Integrating Eq.(14);

$$\int_0^v \frac{dv}{v} = -\frac{1}{R} \int_0^T \frac{Cv}{T} dT$$

$$\rightarrow \ln\left(\frac{v}{v_0}\right) = -\frac{1}{R} \int_0^T \frac{Cv}{T} dT \quad \dots\dots(15)$$

$$\left(\frac{v}{v_0}\right) \equiv Vr = \text{Exp}\left\{-\frac{1}{R} \int_0^T \frac{Cv}{T} dT\right\} \quad \dots\dots(16)$$

Based on Eq.(9);

$$\frac{Cv}{T} dT = \frac{Cp}{T} dT - R \frac{dT}{T}$$

$$\rightarrow \int_0^T \frac{Cv}{T} dT = \int_0^T \frac{Cp}{T} dT - R \int_0^T \frac{dT}{T}$$

$$= (\phi - \phi_0) - R \ln\left(\frac{T}{T_0}\right) \quad \dots\dots(17)$$

Relative volume; Vr may be obtained from Eq.(16) together with Eq.(17) as;

$$Vr = \text{Exp}\left\{-\frac{\phi - \phi_0}{R} + \ln\left(\frac{T}{T_0}\right)\right\} \quad \dots\dots(18)$$

$$Vr \equiv \frac{T}{Pr} \quad \dots\dots(19) \quad \text{will be used in this table.}$$

[3-5] Constant κ Option

Basic equations

$$C_p - C_v = R$$

$$\kappa = 1 / (1 - R/C_p)$$

$\rightarrow (R/C_p) = \text{const. required.}$

$$T_c = 273.15 \text{ (K)}$$

$$R = 0.28703 \text{ {kJ/kg K}} \quad \dots \dots \dots (1)$$

$$C_p = R * \kappa / (\kappa - 1) \quad \dots \dots \dots (2)$$

$$h = C_p T \quad [\text{kJ/kg}] \quad \dots \dots \dots (3)$$

$$u = h - R * T \quad [\text{kJ/kg}] \quad \dots \dots \dots (4)$$

$$\phi = 1 + C_p * \ln(T) \quad [\text{kJ/kg K}] \quad \dots \dots \dots (5)$$

$$s = \phi - R * \ln(P) \quad [\text{kJ/kg K}] \quad \dots \dots \dots (6)$$

$$\begin{aligned} Pr &= \text{Exp}\{(\kappa - 1) / \kappa * \ln(T/T_c)\} \\ &= \text{Exp}\{(\phi - \phi_0) / R\} \quad \dots \dots \dots (7) \end{aligned}$$

-- where $\phi_0 = \phi$ at $T = T_c$

$$V_r = T / Pr \quad \text{defined.} \quad \dots \dots \dots (8)$$

$$T = h / C_p \quad \dots \dots \dots (9)$$

$$T = (h - u) / R \quad \dots \dots \dots (10)$$

$$\begin{aligned} T &= \text{Exp}\{(\kappa - 1) / \kappa * \ln(Pr) + \ln(T_c)\} \quad \dots \dots \dots (11) \\ &= \text{Exp}\{(\kappa - 1) / \kappa * \ln(Pr) + 5.610\} \end{aligned}$$

$$T = \text{Exp}\{k \ln(T_c) - (\kappa - 1) \ln(V_r)\} \quad \dots \dots \dots (12)$$

Table 19 Compressible-Flow Function at $M_n = 1.0$, $T = 300 \text{ (K)}$

κ	C_p	a	T_s/T_t	P_t/P_s	ρ_s/ρ_t	V/\sqrt{T}	Q	Q_s
1.1	3.1573	300.35	0.95238	1.7103	0.61391	17.341	3.7089	6.3435
1.2	1.7222	306.49	0.90909	1.7716	0.62092	17.695	3.8280	6.7815
1.3	1.2438	311.99	0.86957	1.8324	0.62759	18.013	3.9385	7.2170
1.4	1.0046	316.95	0.83333	1.8929	0.63394	18.299	4.0417	7.6506
AIR	1.0028	317.04	0.83293	1.8942	0.63392	18.304	4.0427	7.6564
1.5	0.9611	321.45	0.80000	1.9531	0.64000	18.559	4.1382	8.0824

Note: Example Cal. at $\kappa = 1.2$;

$$(1) \quad a; \quad \text{Sonic velocity} = \sqrt{\kappa R T_s} = \text{Sqt}\{ \kappa R T_t (T_s/T_t) \}$$

$$= \text{Sqt}\{ 1.2 (287.03) 300 (0.90909) \} = 306.49 \text{ [m/sec]}$$

$$(2) \quad V = (V/\sqrt{T}) * \sqrt{T} = 17.695 * \sqrt{300} = 17.695 * 17.3205 = 306.49 = a$$

$$(3) \quad T_s/T_t = 2 / (\kappa + 1), \quad P_t/P_s = \{(\kappa + 1) / 2\}^{**} \{ \kappa / (\kappa - 1) \}, \quad \rho_s/\rho_t = \{2 / (\kappa + 1)\}^{**} \{1 / (\kappa - 1)\}$$

$$(4) \quad \kappa \doteq (2n+3) / (2n+1) \quad \text{where } n = \text{numbers of atomics.}$$

[3-6] Viscosity of Air; μ

Viscosity: μ is arranged in Option: Air
in VB-Version.

The value of μ corresponds to static temperature:
Ts. in Flow function table

Metric unit

Based on Sutherland's equation;

(JSME,Mech. handbook, Vol.5(1968),Sec.10, p.1)

$$\mu = 1.7580 * 10^{-6} \left(\frac{380}{380+t} \right) \left(\frac{273+t}{273} \right)^{\frac{3}{2}}$$

[kg_f sec/m²]-----(1)

The Eq(1) is for T(C), then it was rearranged for T(K)
as below.

$$\mu = 1.7580 * 10^{-6} \left(\frac{380}{380+T-273.15} \right) \left(\frac{T}{273.15} \right)^{\frac{3}{2}} \quad \text{-----}(2)$$

The Eq.(2) shows a slightly different value from Eq.(1).

S I unit

$$1 \left(\frac{\text{kg}_f \text{ sec}}{\text{m}^2} \right) = \frac{9.80665(\text{N}) \text{ sec}}{\text{m}^2} = 9.80665 \quad [\text{Pa sec}] \quad \text{-----}(3)$$

Note that:

$$1 [\text{kg}_f] = 9.80665 (\text{N}), \quad 1 (\text{N}/\text{m}^2) = 1 [\text{Pa}]$$

$$1 [\text{kg}_f \text{ sec} / \text{m}^2] = 9.80665 [\text{Pa sec}]$$

British unit

$$1 \left(\frac{\text{kg}_f \text{ sec}}{\text{m}^2} \right) = \frac{\left(\frac{1}{0.453592} \right) [\text{lb sec}]}{\left(\frac{1}{0.3048} \right)^2 [\text{ft}^2]} = \frac{(0.3048)^2}{0.453592} = 0.2048163 \quad \left[\frac{\text{lb}_f \text{ sec}}{\text{ft}^2} \right] \quad \text{-----}(4)$$

Note that:

$$1 [\text{lb}_f] = 0.453592 [\text{kg}_f], \quad 1 [\text{ft}] = 0.3048 [\text{m}]$$

$$1 [\text{lb}_f \text{ sec}/\text{ft}^2] = 32.17404 [\text{lb}_m/\text{ft sec}]$$

SUMMARY

$$[\mu]_{\text{Metric}} \text{ obtainable from Eq.(2)} \cdots [\text{kg}_f \text{ sec}/\text{m}^2]$$

$$[\mu]_{\text{SI}} = 9.80665 * [\mu]_{\text{Metric}} \cdots [\text{Pa sec}]$$

$$[\mu]_{\text{British}} = 0.2048163 * [\mu]_{\text{Metric}} \cdots [\text{lb}_f \text{ sec}/\text{ft}^2]$$

--- for T(R)=1.8*T(K)

(Ref.): Sutherland's equation for British unit:

$$\mu * 10^6 = (0.3170 * 10^{-4}) * T_r^{1.5} * \left(\frac{734.6}{T_r + 216} \right) \quad [\text{lb}_f \text{ sec}/\text{ft}^2] \cdots (5)$$

[Notes]

Kinematic Viscosity; ν

Viscosity; μ will be obtained as below from
the Option :Air in VB-Version at T=288.15(K).

$$\mu = 17.97 * 10^{-6} [\text{Pa sec}] \text{ or } \{\text{kg}_m/\text{m sec}\}$$

---for SI unit

$$\mu = 1.832 * 10^{-6} [\text{kg}_f \text{ sec}/\text{m}^2] \text{ ---for Metric unit}$$

At T=518.67 (R);

$$\mu = 0.3753 * 10^{-6} [\text{lb}_f \text{ sec}/\text{ft}^2] \text{ ---for British unit.}$$

Kinematic Viscosity: ν will be obtained as;

$$\nu = \mu / \rho [\text{m}^2/\text{sec}]$$

where:

$$\rho = P/RT = [\text{Pa}/(\text{J}/\text{kg}_m \text{ K}) * \text{K}]$$

$$= 0.1013 * 10^6 / (287 * 288.15) = 1.2249 [\text{kg}_m/\text{m}^3]$$

$$\therefore \nu = \mu / \rho = 17.97 * 10^{-6} / 1.2249$$

$$= 14.67 * 10^{-6} [\text{m}^2/\text{sec}]$$

[4-3] **FLtbl1** Table 22 Air Flow Table at T=288.15 (SI unit)

Mn	Ps/Pt	Pt/Ps	Ts/Tt	RO/ROt	V/RTt	ND= 1	T= 288.150	F= .00000
						Q	Qs	A/Ach
.000	1.00000	1.0000	1.00000	1.00000	.00000	.00000	.00000	.00000
.100	.99303	1.0070	.99800	.99502	2.00311	.69440	.69928	5.82145
.120	.98998	1.0101	.99712	.99284	2.40272	.83111	.83952	4.86389
.140	.98639	1.0138	.99609	.99027	2.80174	.96662	.97996	4.18202
.160	.98227	1.0180	.99490	.98731	3.20008	1.10076	1.12062	3.67241
.180	.97763	1.0229	.99355	.98398	3.59765	1.23334	1.26155	3.27764
.200	.97248	1.0283	.99205	.98028	3.99439	1.36419	1.40279	2.96325
.220	.96683	1.0343	.99039	.97620	4.39018	1.49314	1.54437	2.70736
.240	.96068	1.0409	.98859	.97177	4.78493	1.62000	1.68631	2.49534
.260	.95406	1.0482	.98663	.96698	5.17859	1.74464	1.82866	2.31707
.280	.94697	1.0560	.98453	.96185	5.57102	1.86689	1.97143	2.16535
.300	.93943	1.0645	.98228	.95638	5.96216	1.98660	2.11468	2.03487
.320	.93146	1.0736	.97989	.95058	6.35193	2.10363	2.25842	1.92167
.340	.92307	1.0833	.97735	.94446	6.74022	2.21786	2.40269	1.82270
.360	.91428	1.0938	.97468	.93803	7.12698	2.32915	2.54753	1.73562
.380	.90510	1.1049	.97187	.93129	7.51213	2.43740	2.69297	1.65854
.400	.89555	1.1166	.96892	.92427	7.89555	2.54248	2.83902	1.58999
.420	.88565	1.1291	.96585	.91697	8.27722	2.64432	2.98574	1.52876
.440	.87542	1.1423	.96264	.90939	8.65703	2.74282	3.13315	1.47386
.460	.86487	1.1562	.95931	.90156	9.03492	2.83789	3.28128	1.42449
.480	.85403	1.1709	.95585	.89348	9.41081	2.92947	3.43016	1.37997
.500	.84292	1.1864	.95227	.88516	9.78463	3.01748	3.57981	1.33972
.520	.83154	1.2026	.94857	.87662	10.15632	3.10188	3.73028	1.30327
.540	.81993	1.2196	.94476	.86787	10.52582	3.18263	3.88159	1.27021
.560	.80810	1.2375	.94084	.85891	10.89305	3.25968	4.03376	1.24019
.580	.79607	1.2562	.93681	.84977	11.25798	3.33301	4.18684	1.21290
.600	.78386	1.2757	.93267	.84044	11.62053	3.40260	4.34084	1.18810
.620	.77149	1.2962	.92843	.83096	11.98065	3.46844	4.49580	1.16555
.640	.75897	1.3176	.92409	.82131	12.33829	3.53052	4.65173	1.14506
.660	.74633	1.3399	.91966	.81152	12.69339	3.58885	4.80869	1.12645
.680	.73358	1.3632	.91513	.80161	13.04591	3.64345	4.96668	1.10958
.700	.72074	1.3875	.91052	.79157	13.39581	3.69432	5.12574	1.09430
.720	.70783	1.4128	.90582	.78143	13.74303	3.74151	5.28589	1.08050
.740	.69486	1.4391	.90103	.77118	14.08753	3.78503	5.44716	1.06808
.760	.68186	1.4666	.89617	.76086	14.42929	3.82493	5.60957	1.05694
.780	.66883	1.4951	.89123	.75045	14.76825	3.86126	5.77315	1.04700
.800	.65580	1.5249	.88622	.73999	15.10438	3.89407	5.93793	1.03818
.820	.64277	1.5558	.88115	.72947	15.43766	3.92341	6.10394	1.03042
.840	.62976	1.5879	.87600	.71890	15.76805	3.94934	6.27118	1.02366
.860	.61679	1.6213	.87079	.70831	16.09552	3.97194	6.43970	1.01784
.880	.60387	1.6560	.86553	.69768	16.42005	3.99126	6.60951	1.01292
.900	.59100	1.6920	.86021	.68705	16.74162	4.00739	6.78063	1.00884
.920	.57822	1.7295	.85483	.67641	17.06019	4.02039	6.95310	1.00558
.940	.56551	1.7683	.84941	.66577	17.37576	4.03036	7.12692	1.00310
.960	.55290	1.8086	.84394	.65514	17.68831	4.03737	7.30214	1.00136
.980	.54040	1.8505	.83843	.64454	17.99783	4.04151	7.47876	1.00033
1.000	.52801	1.8939	.83288	.63396	18.30428	4.04287	7.65680	1.00000
1.100	.46808	2.1364	.80462	.58174	19.79044	4.01108	8.56918	1.00794
1.200	.41212	2.4265	.77580	.53122	21.19938	3.92348	9.52029	1.03045
1.300	.36068	2.7725	.74673	.48302	22.53137	3.79162	10.51240	1.06629
1.400	.31404	3.1843	.71769	.43758	23.78762	3.62646	11.54758	1.11486
1.500	.27236	3.6716	.68854	.39557	24.96276	3.44025	12.63114	1.17550
1.600	.23525	4.2509	.66023	.35631	26.07421	3.23678	13.75911	1.24937
1.700	.20258	4.9362	.63255	.32026	27.11712	3.02572	14.93559	1.33650
1.800	.17405	5.7456	.60562	.28738	28.09460	2.81295	16.16203	1.43757
1.900	.14926	6.6997	.57954	.25755	29.00993	2.60304	17.43966	1.55348
2.000	.12784	7.8224	.55438	.23060	29.86650	2.39946	18.76964	1.68527
3.000	.02728	36.6516	.35612	.07661	35.90676	.95843	35.12816	4.21891
4.000	.00662	151.0994	.23731	.02789	39.08175	.37973	57.37761	10.64819
5.000	.00190	525.0594	.16607	.01147	40.86720	.16329	85.73722	24.76236
6.000	.00064	1562.6190	.12149	.00527	41.94574	.07698	120.28880	52.52660
7.000	.00024	4086.8010	.09223	.00265	42.63882	.03941	161.06680	102.59550
8.000	.00010	9615.0800	.07217	.00144	43.10745	.02164	208.08750	186.83450
9.000	.00005	20738.5300	.05790	.00083	43.43782	.01260	261.35920	320.84080
10.000	.00002	41621.6100	.04742	.00051	43.67884	.00771	320.88640	524.46610